

# Thermal Management for Buck Converters Using Co-Packaged GaN Power HEMTs

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## Speaker: Gaoqiang Deng

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**Current research interest: Power devices (IGBTs, LDMOST, GaN HEMTs)**

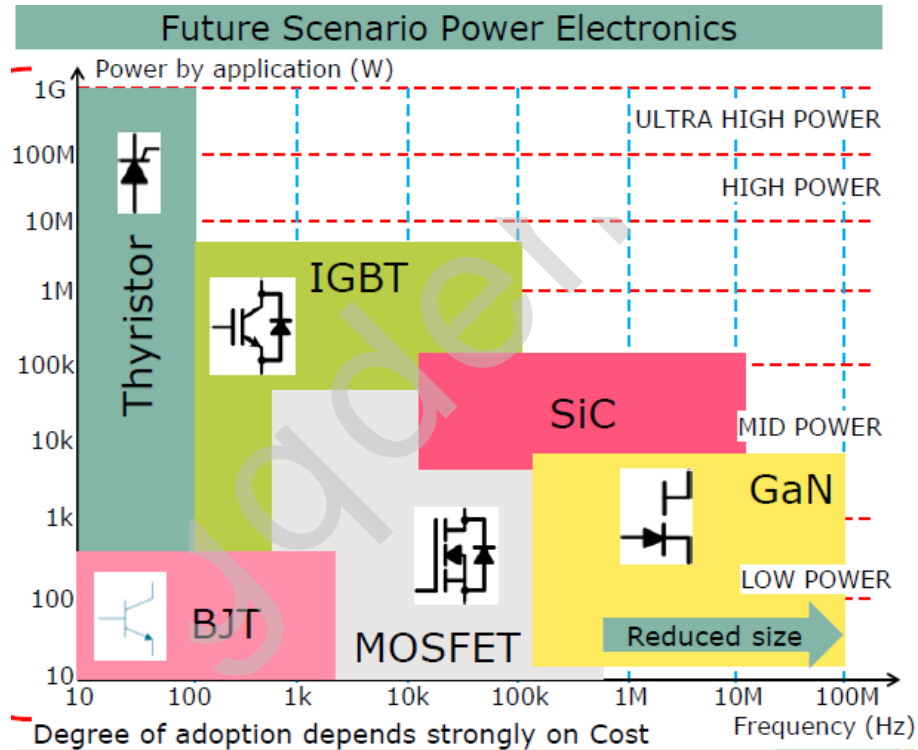
<b>2015 – Present</b>	<b>Ph.D.</b>	<b>Electrical Engineering</b>	<b>UESTC</b>
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<b>2011 – 2015</b>	<b>B.A.Sc.</b>	<b>Electrical Engineering</b>	<b>UESTC</b>



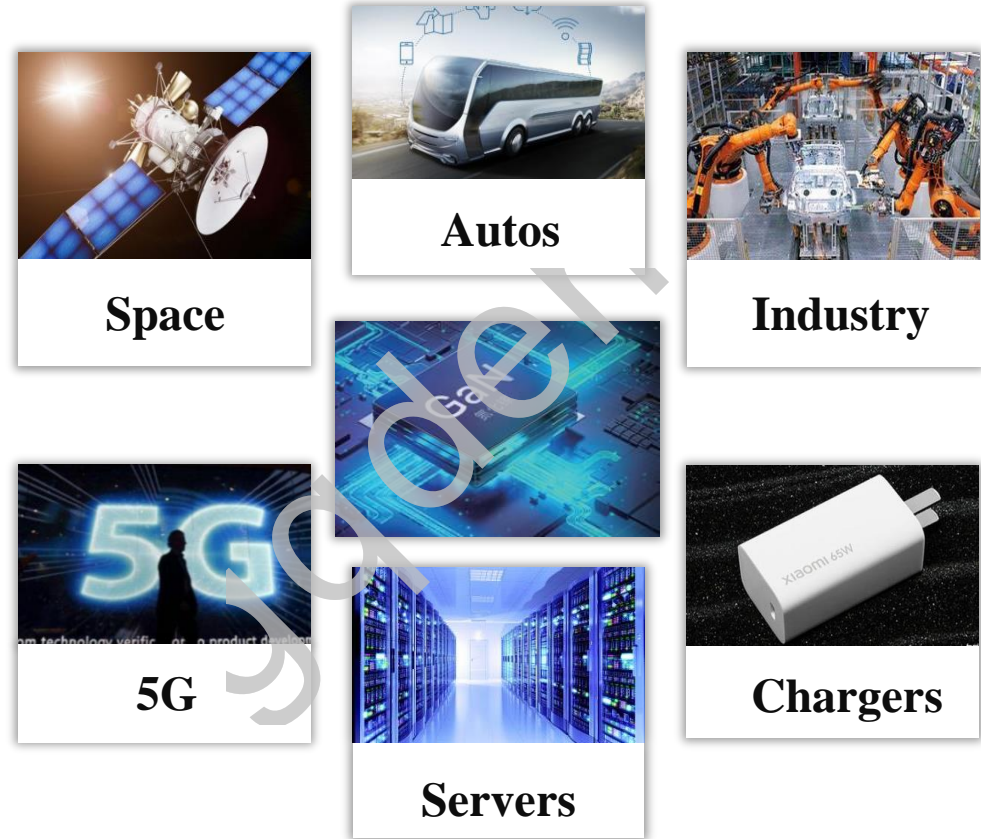
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- 1 Introduction**
- 2 Proposed GaN Power Module**
- 3 Thermal Considerations for Modules**
- 4 Conclusions and Future Work**

## Applications for GaN devices



**Low / medium power, High frequency**



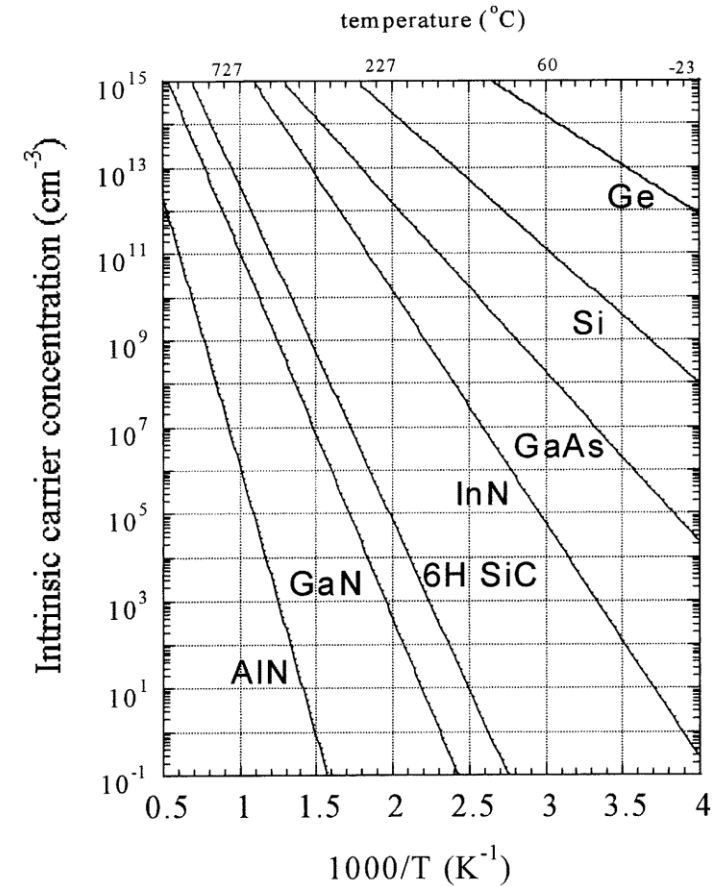
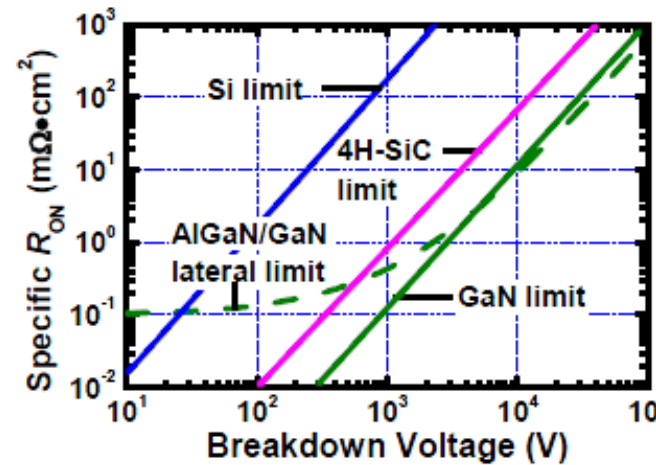
**Market size will be \$300M in 2021 and \$424M in 2023, estimated by Yole Développement.**



# 1. Introduction

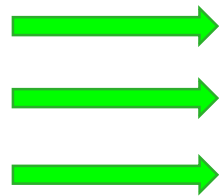
GaN power devices break the performance limit of Silicon power devices!

Material	Critical Field $E_{crit}$ (MV/cm)	Electron Mobility $\mu_n$ (cm <sup>2</sup> /Vs)	Band gap $E_g$ (eV)
Silicon	0.3	1400	1.12
SiC	2.2	700	3.25
GaN(HEMT)	3.3	1800 (2DEG)	3.44



**Material**

- High Critical Field
- High Mobility
- Wide Band gap



**Devices**

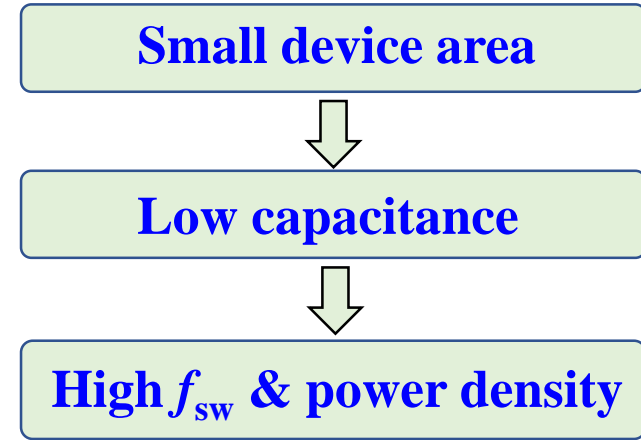
- High BV
- Low  $R_{on,sp}$
- High  $T_j$

S.M.Sze, "Physics of Semiconductor devices", Chapter 1

## GaN-based power conversion systems



Device size comparison



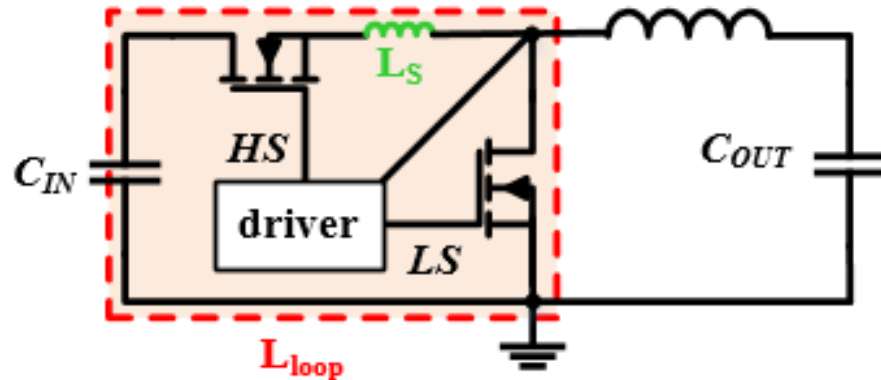
System comparison

- Frequency **2.7×**
- Volume **34%**
- Power Density **2.8×**

Source: Infineon\_CoolGaN\_ProductSelectionGuide.2019

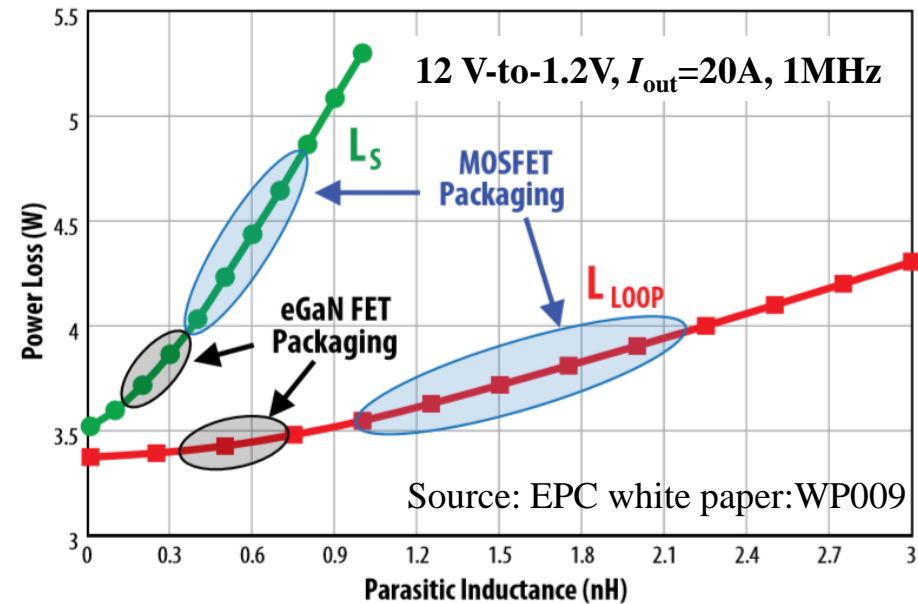
## Packaging matters !

- Less parasitic inductance and resistance
- Lower thermal impedance
- Smaller footprint and physical size



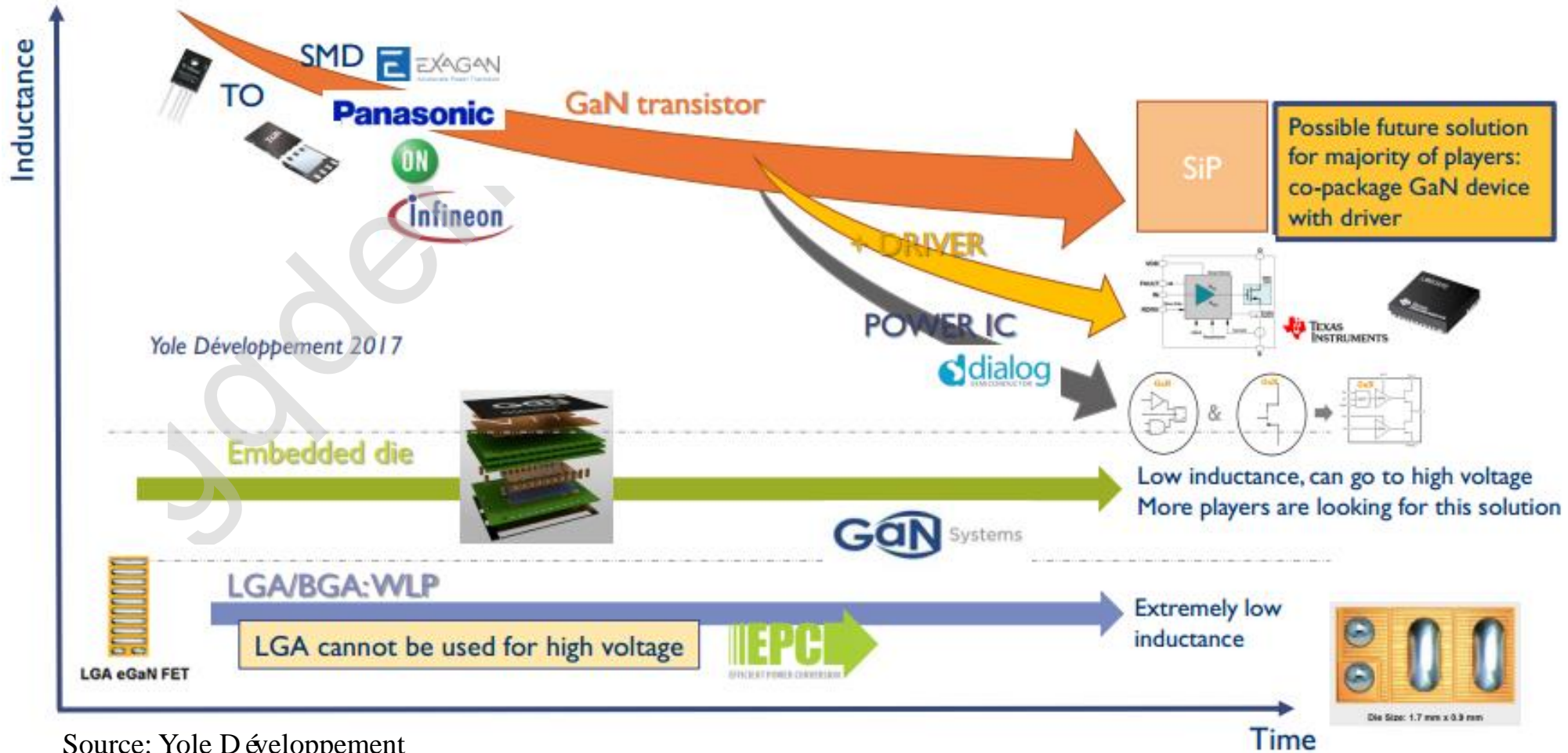
Synchronous buck converter with parasitic inductances

The higher the device frequency, the more important the consequences of parasitic inductance.



Parasitic inductance impact on power loss

## Packaging roadmap for GaN transistors



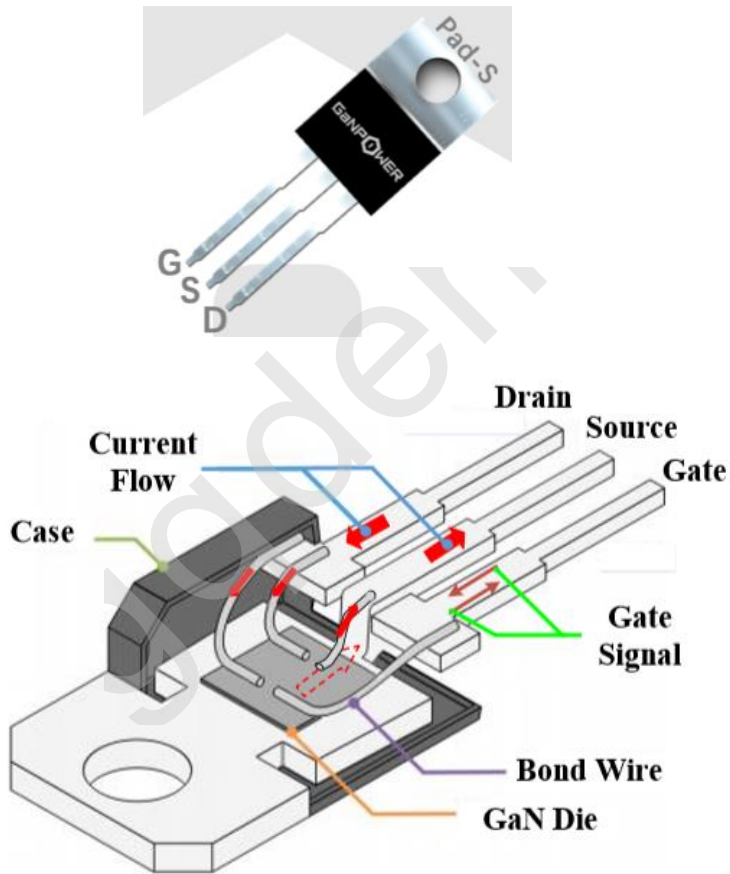
Source: Yole Développement



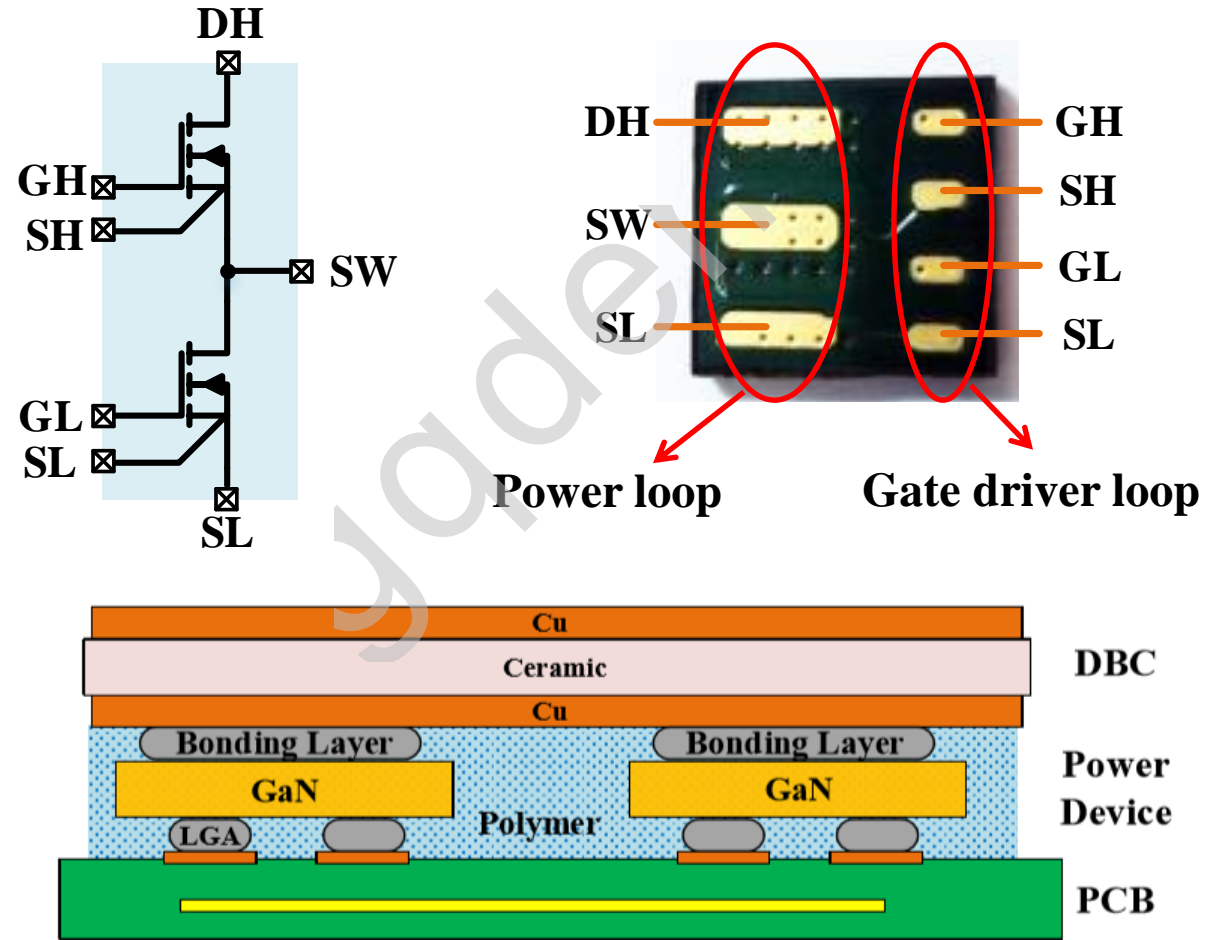
- 1 Introduction
- 2 **Proposed GaN Power Module**
- 3 Thermal Considerations for Modules
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# 2. Proposed GaN Power Module

## GaN transistor in TO-220 package



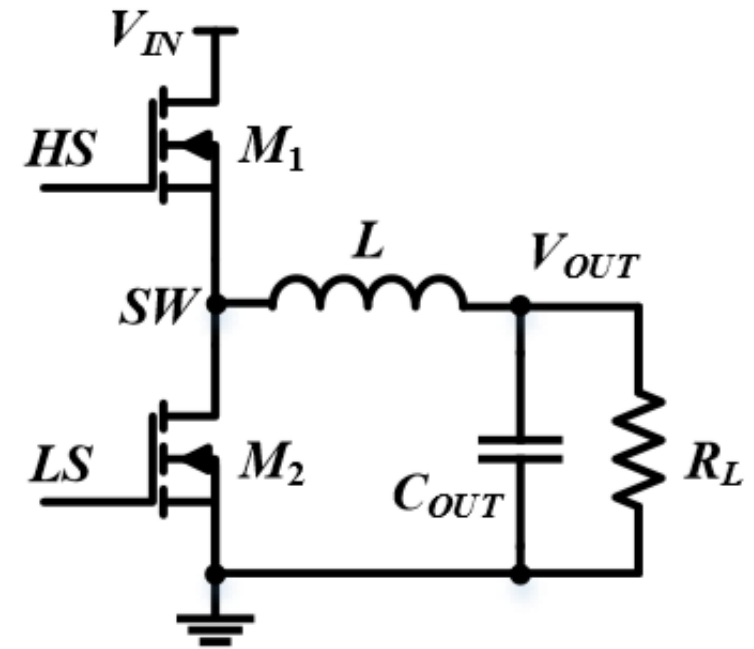
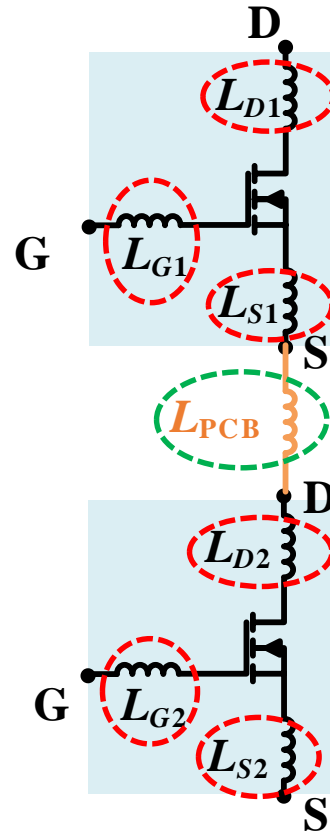
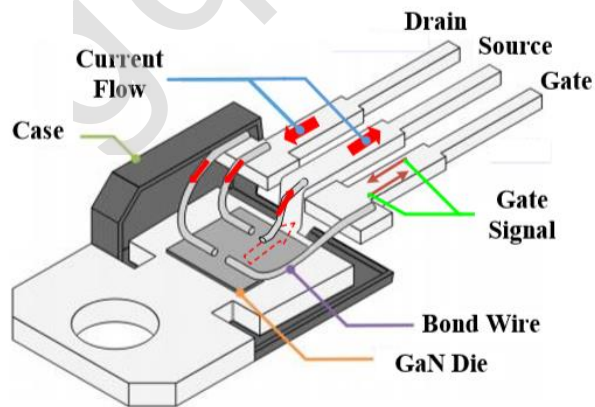
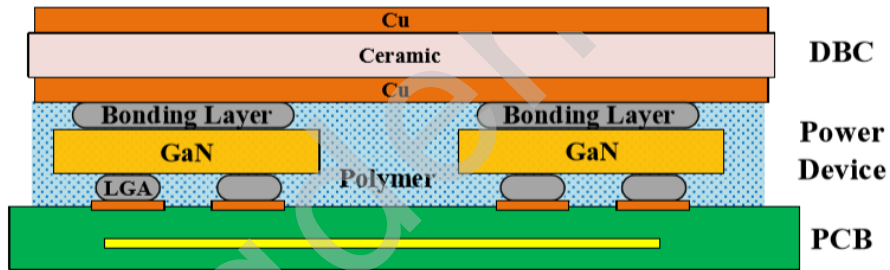
## Custom Half-Bridge Module for this work



# 2. Proposed GaN Power Module

## How the GaN power modules minimize the parastics:

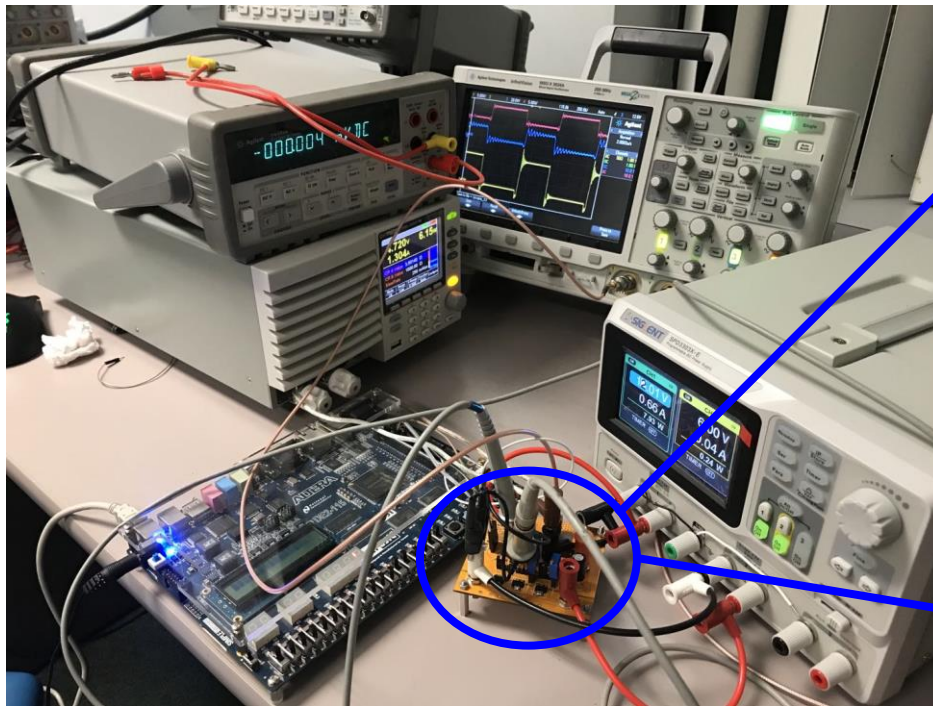
- Eliminate bond wire by flip-chip assembly
- Shorten the wire connection on PCBs by co-packaging



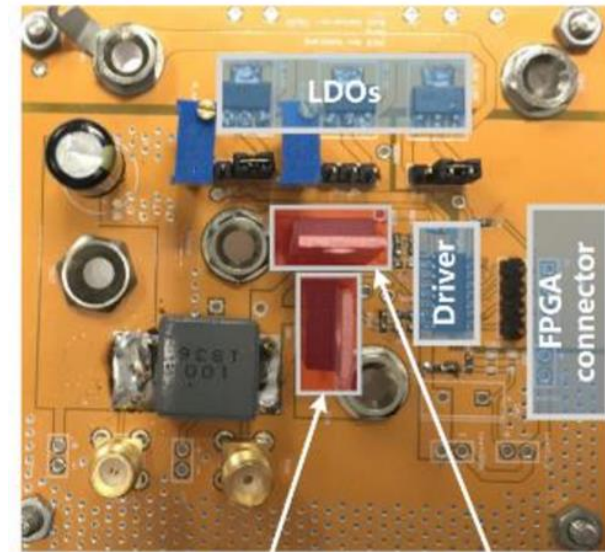
# 2. Proposed GaN Power Module

## Experimental setup

- System is tested with 2 different setups
  - Custom power module
  - Two standard TO-220 packages



GaN Power Module



HS GaN HEMT

LS GaN HEMT



## 2. Proposed GaN Power Module

### □ Component list for the test PCB

Component	Value	No.	Model number	Description
Module	15A	1	Custom prototype	Switch
HEMT	15A	2	GPI65015TO	Switch
Driver	4A	1	Si8273	Gate driver
Inductor	10 $\mu$ H	1	SRP1265A-100M	Filter inductor
Capacitor	220 $\mu$ F	1	EEU-FM1V221L	Filter capacitor
LDO	Adjustable	2	NCP1117STAT3G	Power for drivers
Diode	100V	1	MBR1H100SFT3G	Bootstrap diode

### □ Apparatus used for the test

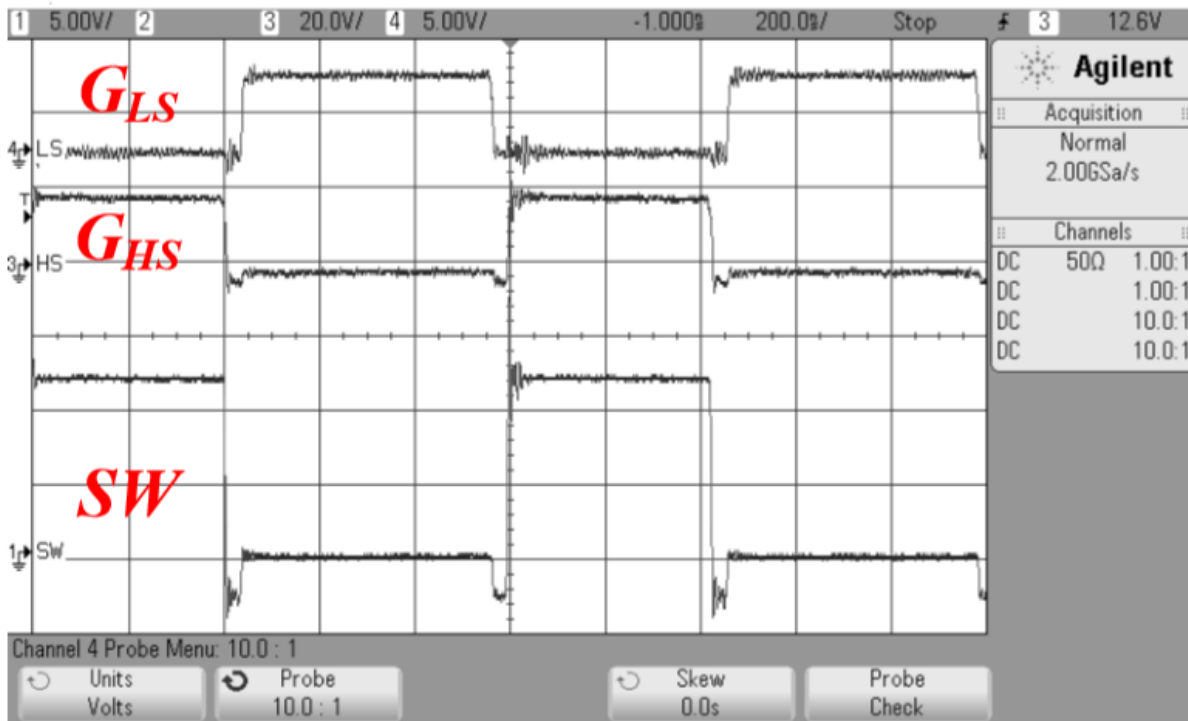
Oscilloscope: *Agilent Technologies MSO-X 3024A*

DC Power Supply: *SIGLENT SPD3303X-E*

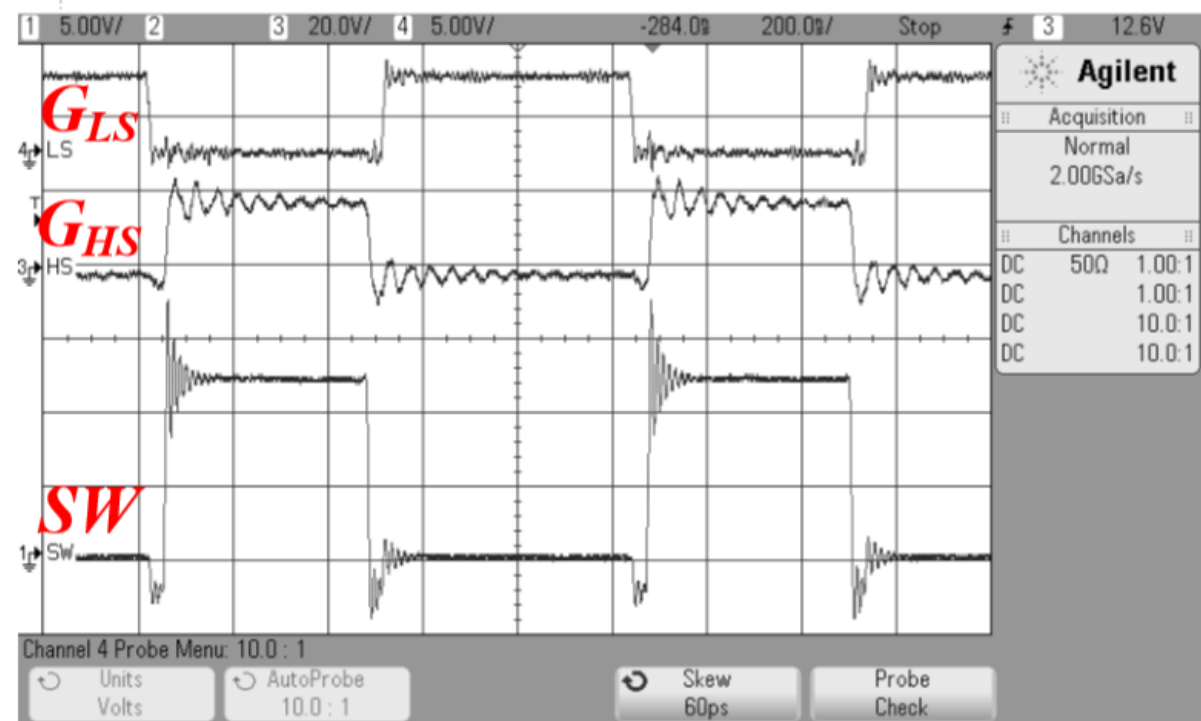
DC Electronic Load: *GWINSTEK PEL-3031E*

## Experimental results

□ Waveforms comparison (Buck converter,  $V_{IN} = 12\text{ V}$ ,  $V_{OUT} = 5\text{ V}$ ,  $f = 1\text{ MHz}$ )



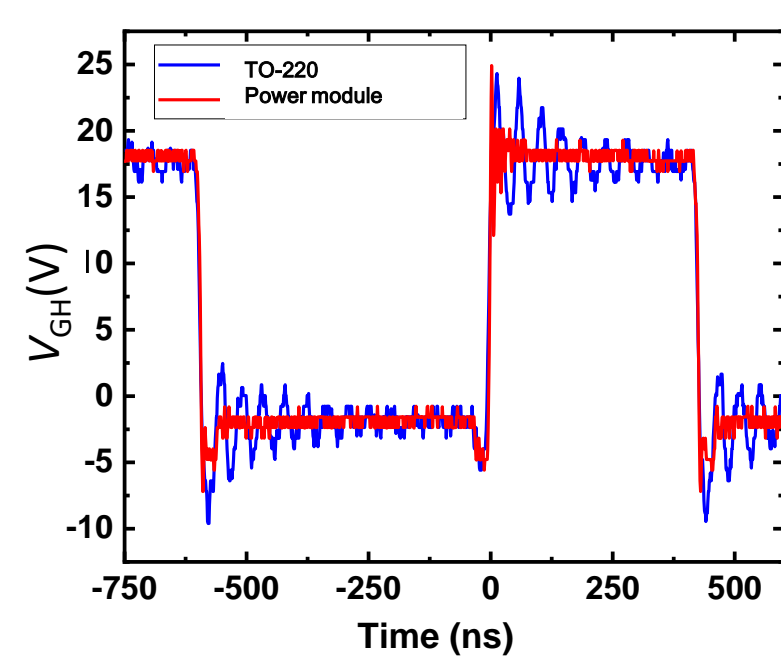
GaN power module



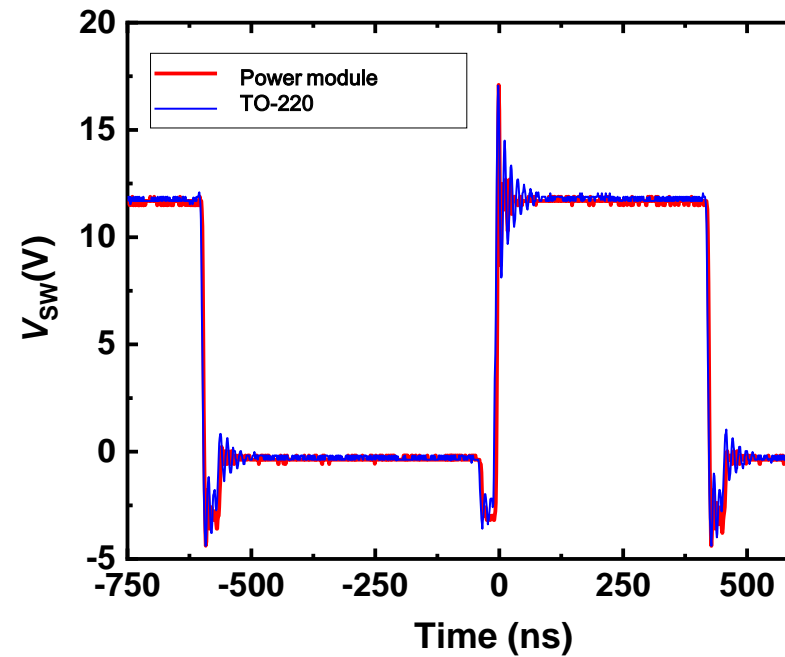
TO-220 packages

## Experimental results

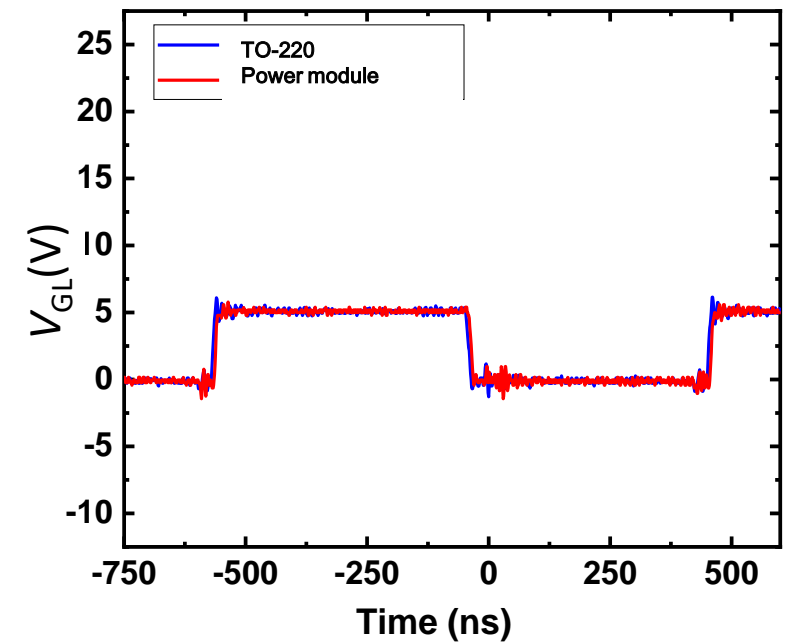
□ Waveforms comparison (Buck converter,  $V_{IN} = 12\text{ V}$ ,  $V_{OUT} = 5\text{ V}$ ,  $f = 1\text{ MHz}$ )



Waveforms at HS gates



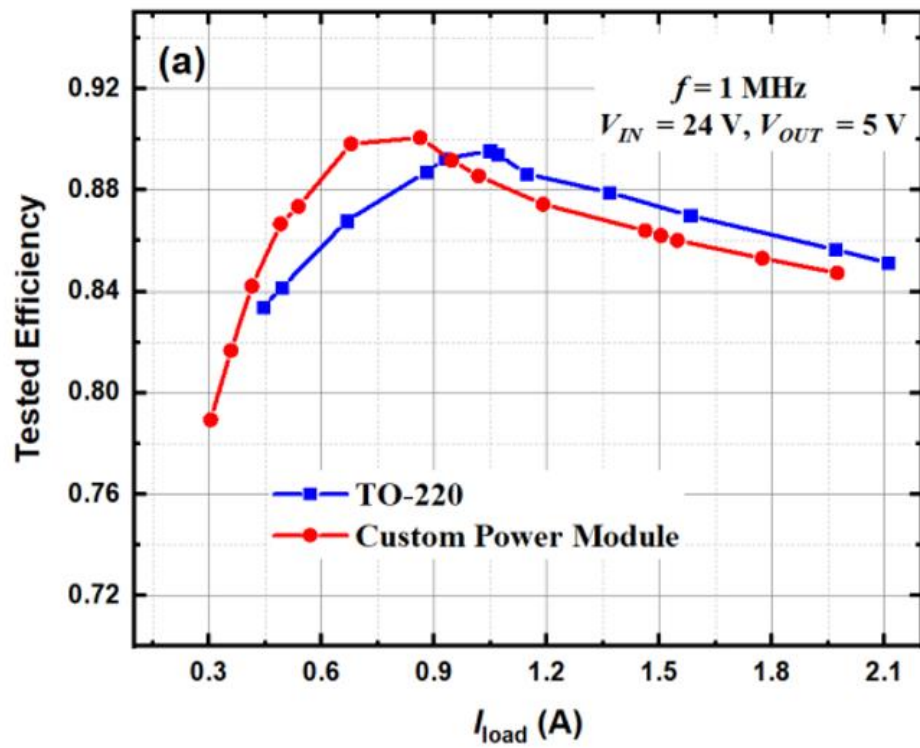
Waveforms at switching nodes



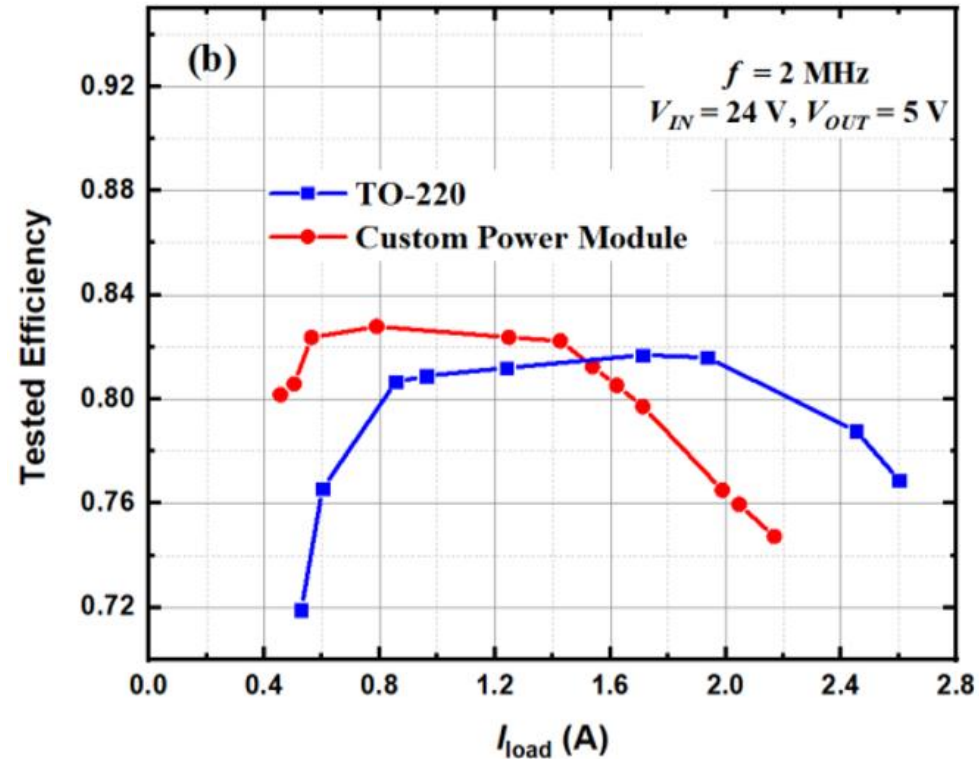
Waveforms at LS gates

## Experimental results

- Efficiency plot (Buck converter,  $V_{IN} = 24\text{ V}$ ,  $V_{OUT} = 5\text{ V}$ , Dead-time 40ns)



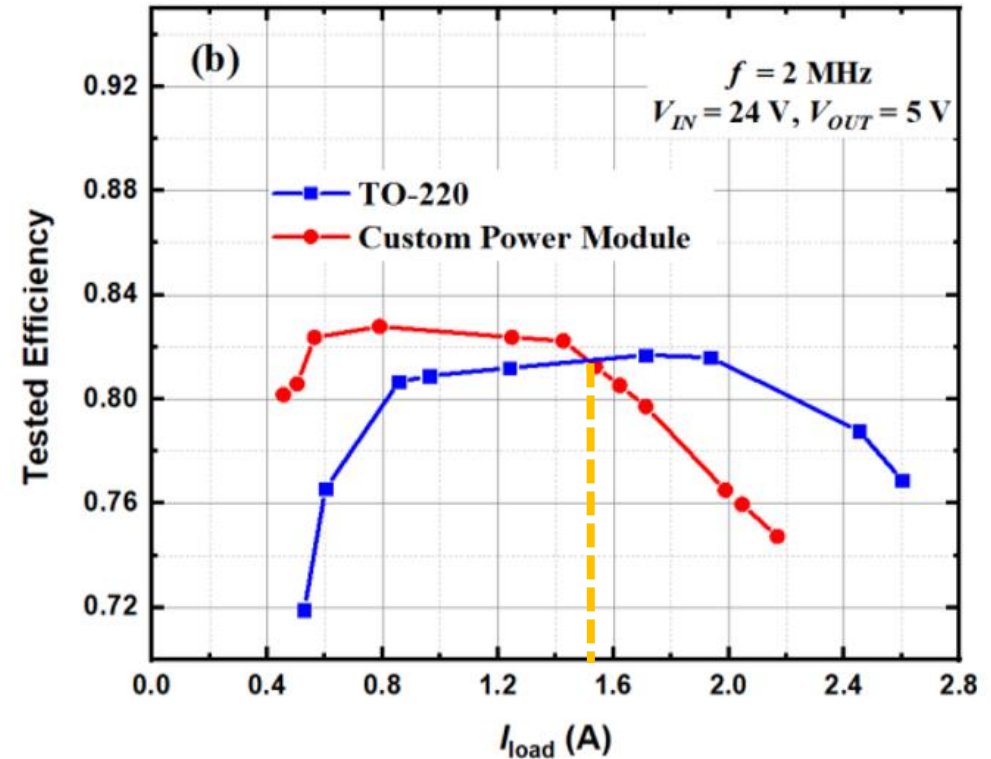
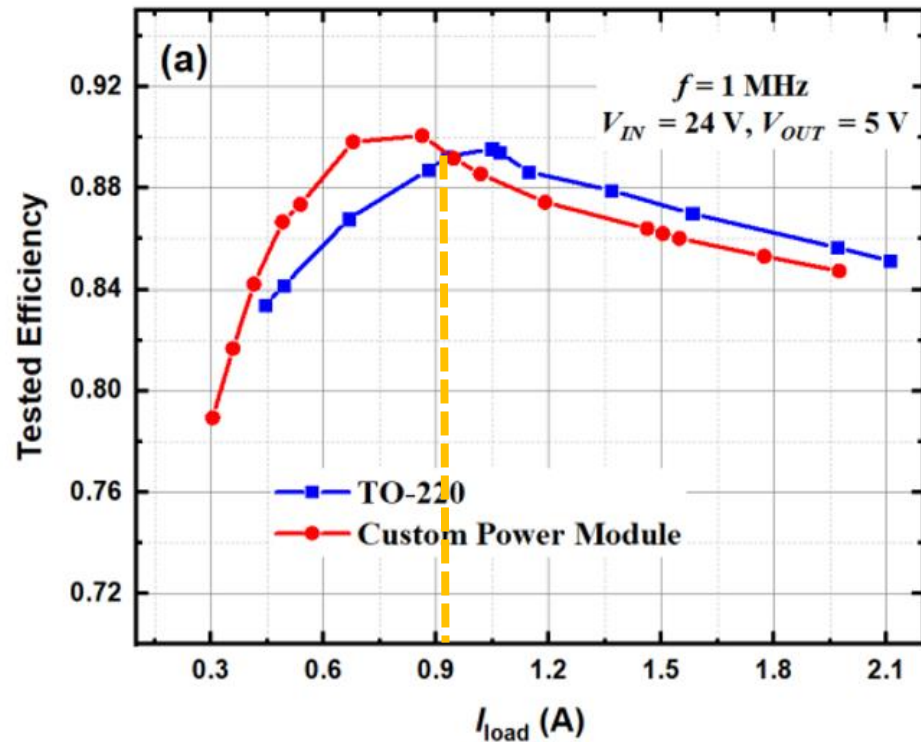
$f = 1\text{ MHz}$



$f = 2\text{ MHz}$



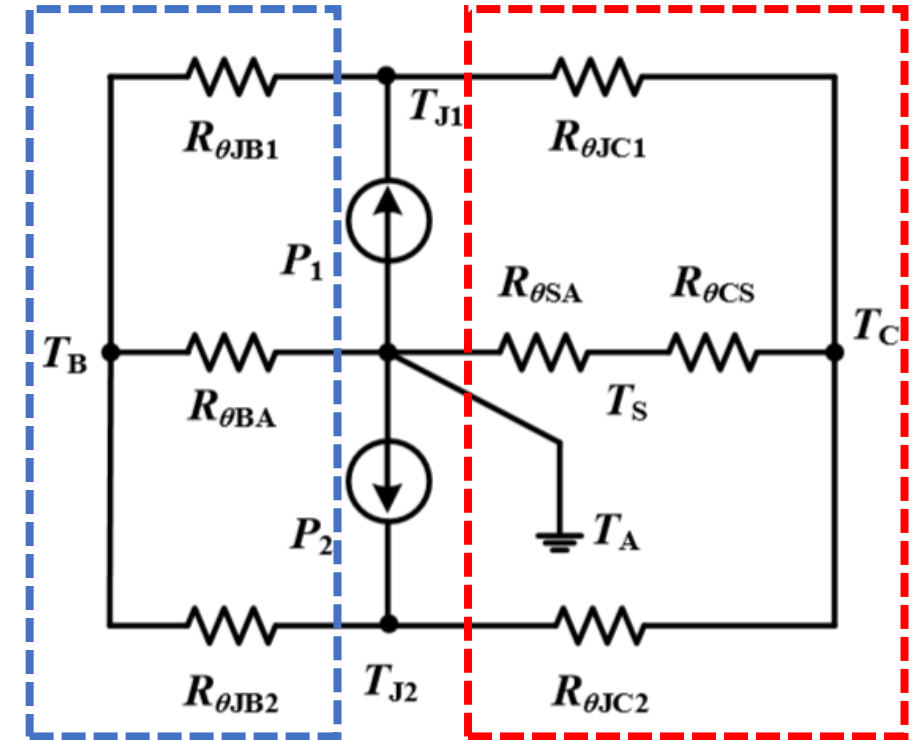
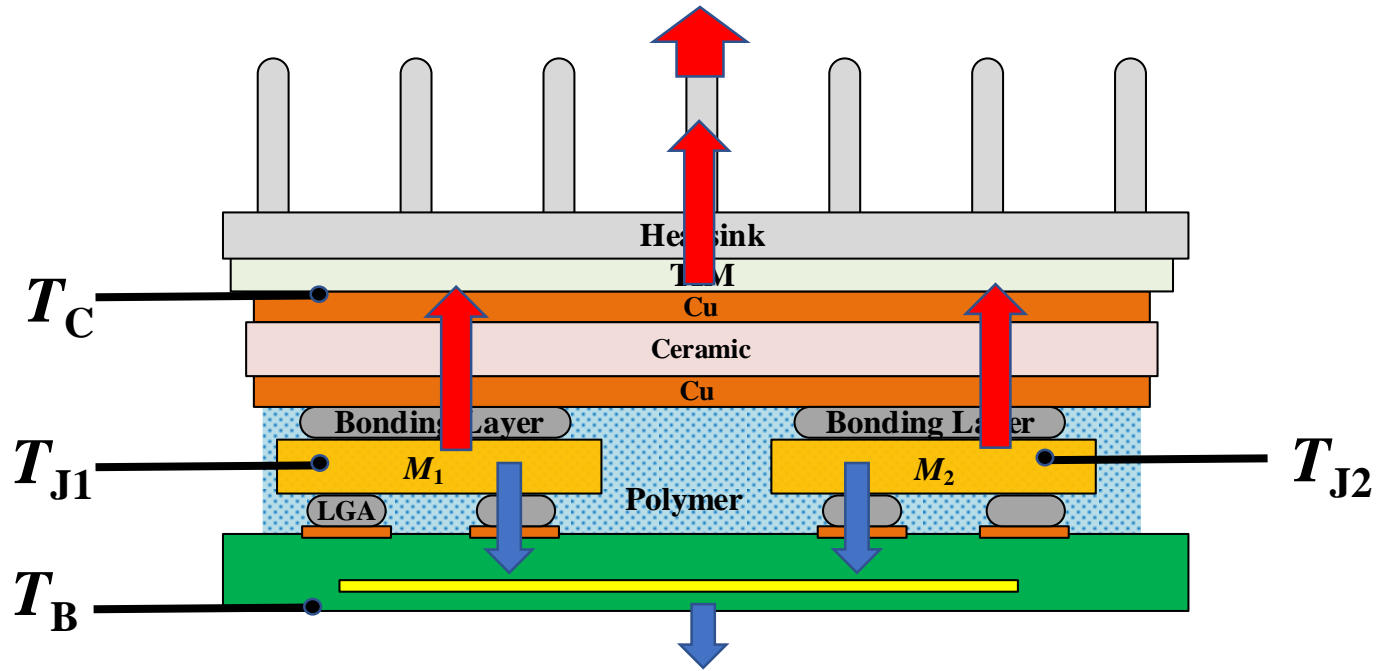
# 2. Proposed GaN Power Module



- **Light load:** Power module shows higher efficiencies owing to suppressed ringing oscillation
- **Heavy load:** Power module shows lower efficiencies owing to large heat transfer
- **The higher the switching frequency, the more advantageous the power module will be!**

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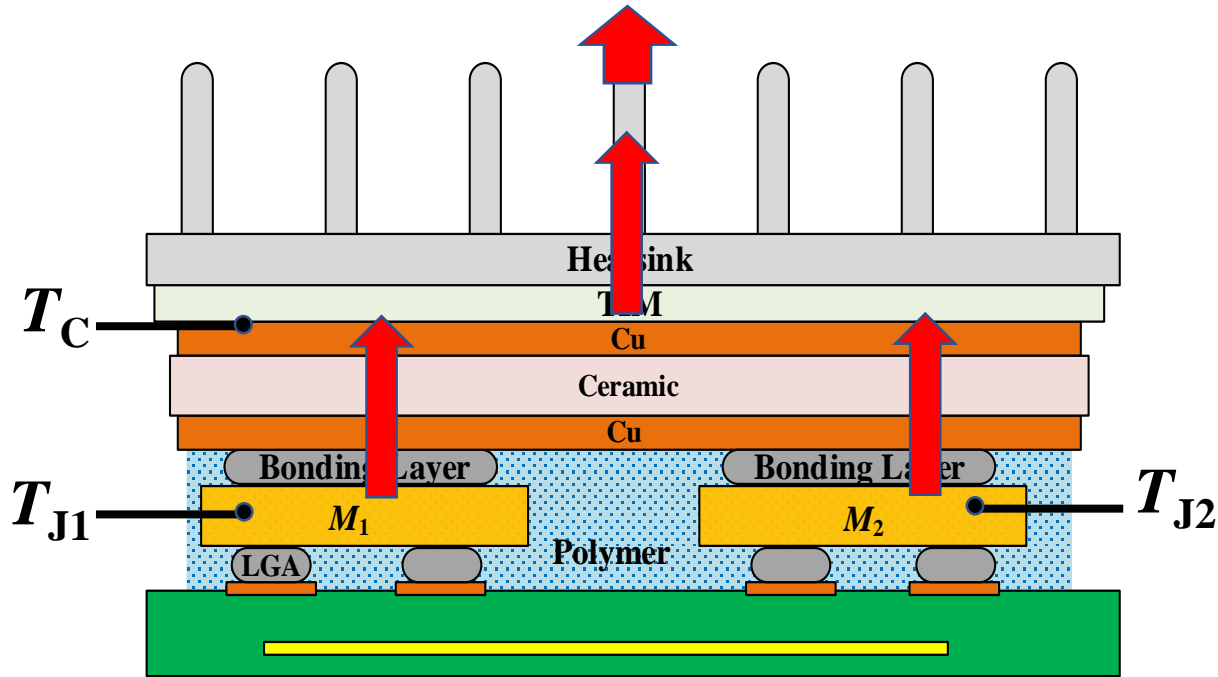
## Thermal equivalent circuit



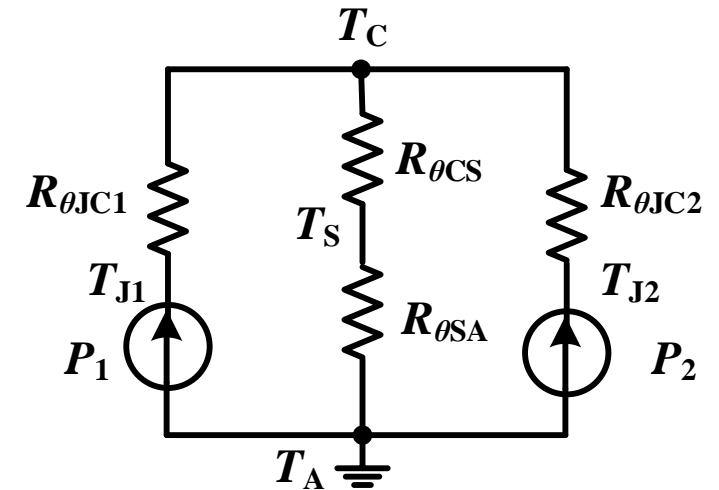
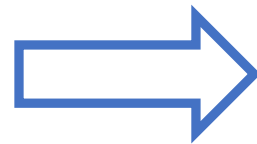
**Upwards: Junction-to-Case ( $R_{\theta JC}$ ), Case-to-Sink ( $R_{\theta CS}$ ), Sink-to-Ambient ( $R_{\theta SA}$ )**

**Downwards: Junction-to-Board ( $R_{\theta JB}$ ), Board-to-Ambient ( $R_{\theta BA}$ )**

## Simplified thermal equivalent circuit



**Heat mainly dissipates upwards !**



$$T_{J1} = DP_{\text{switch}}R_{\theta JC1} + T_C$$

$$T_{J2} = (1 - D)P_{\text{switch}}R_{\theta JC2} + T_C$$

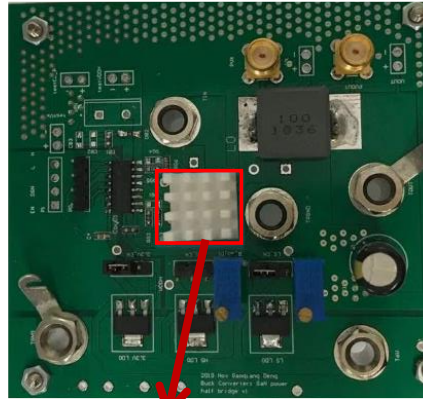
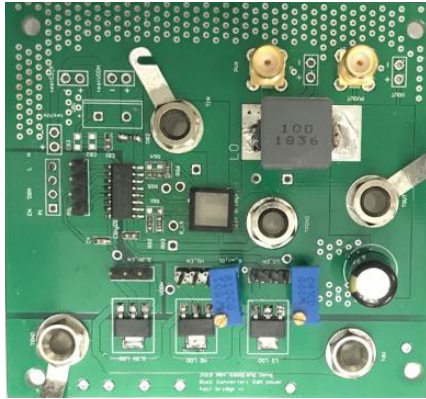
$$T_C = R_{\theta CA}P_{\text{switch}} + T_A$$

$$R_{\theta CA} = R_{\theta CS} + R_{\theta SA}$$

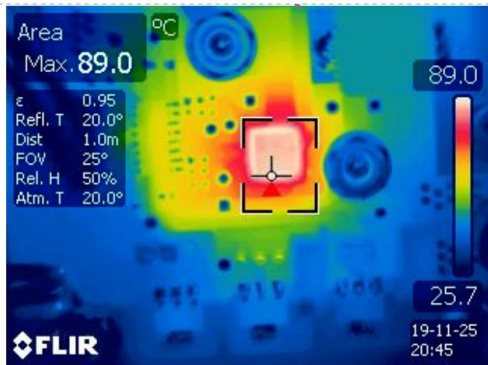
$$T_S = R_{\theta SA}P_{\text{switch}} + T_A$$



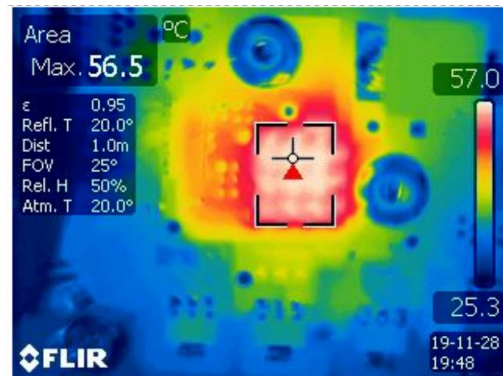
## Measuring $R_{\theta CA}$ & $R_{\theta SA}$



Top-mount ceramic heatsink (TG-CJP-12-LI98)

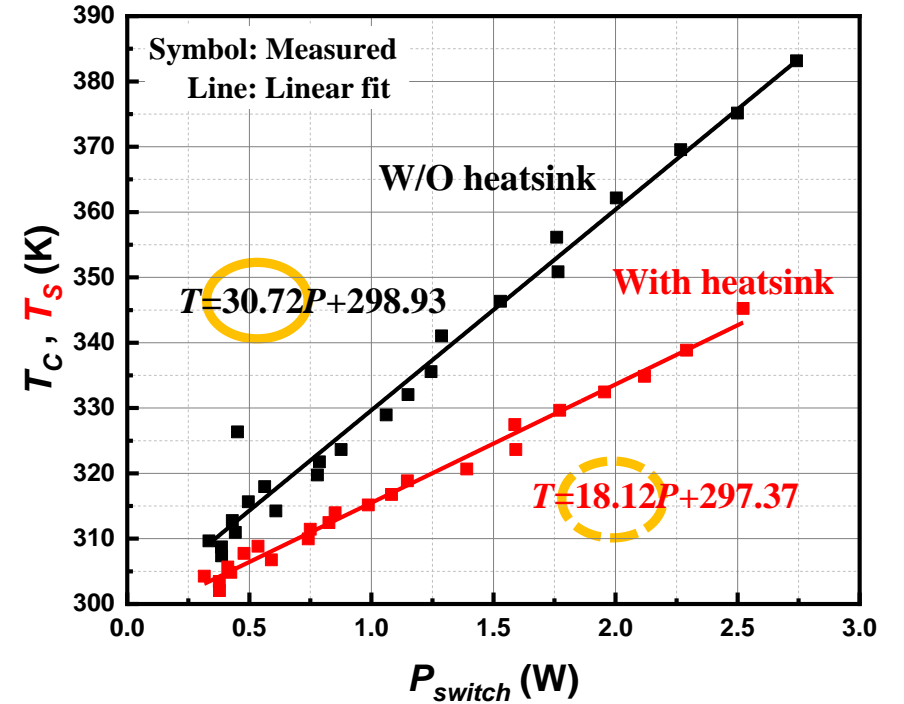


Without a heatsink



With a heatsink

Convection cooling, Output power 9 W

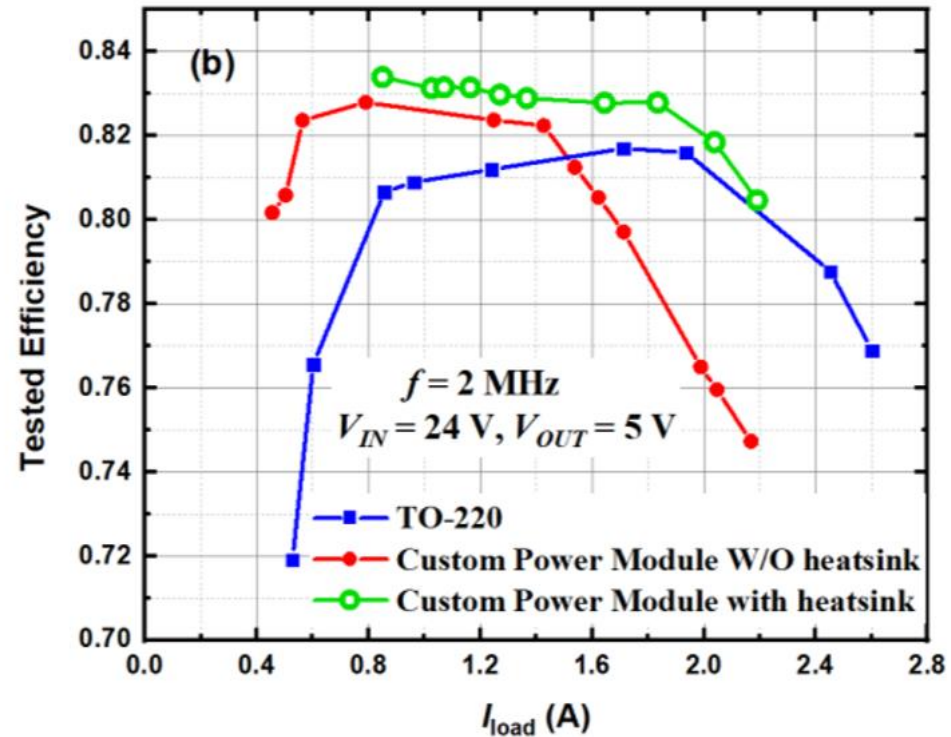
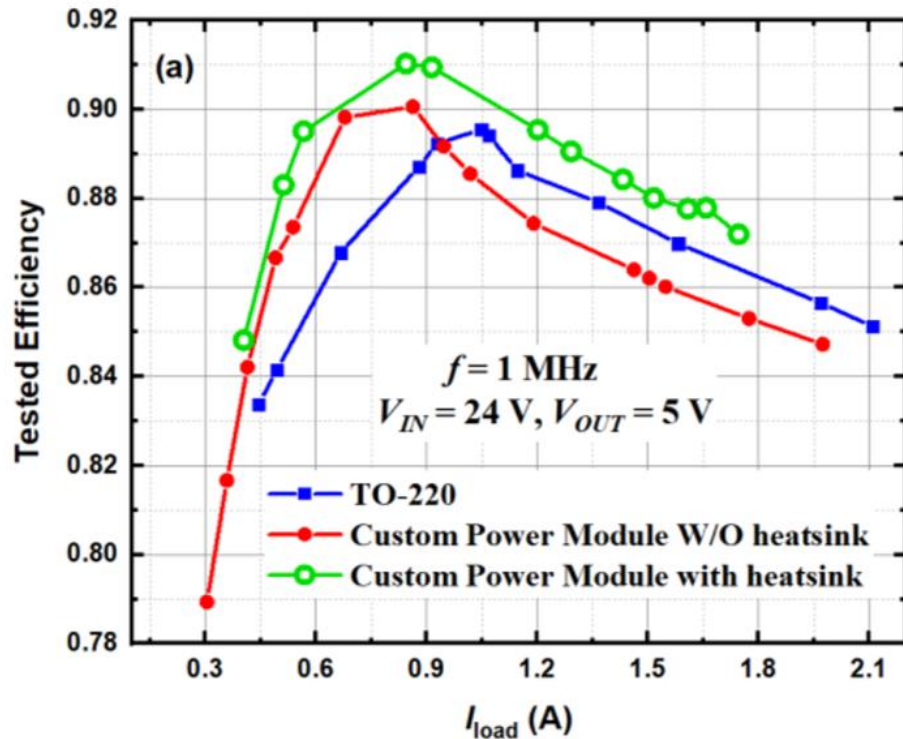


$$P_{switch} = P_{in} - P_{load} - P_{ESR} - P_L$$

$$T_C = R_{\theta CA} P_{switch} + T_A$$

$$T_S = R_{\theta SA} P_{switch} + T_A$$

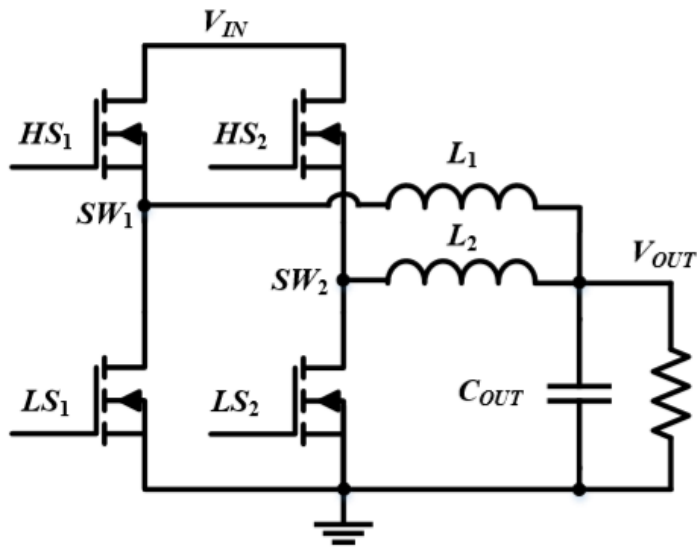
**Efficiency plot** (Buck converter,  $V_{IN} = 24\text{ V}$ ,  $V_{OUT} = 5\text{ V}$ , Dead-time 40ns)



**Improved efficiency at heavy load due to decreased junction temperature!**

## Multi-phase buck converter

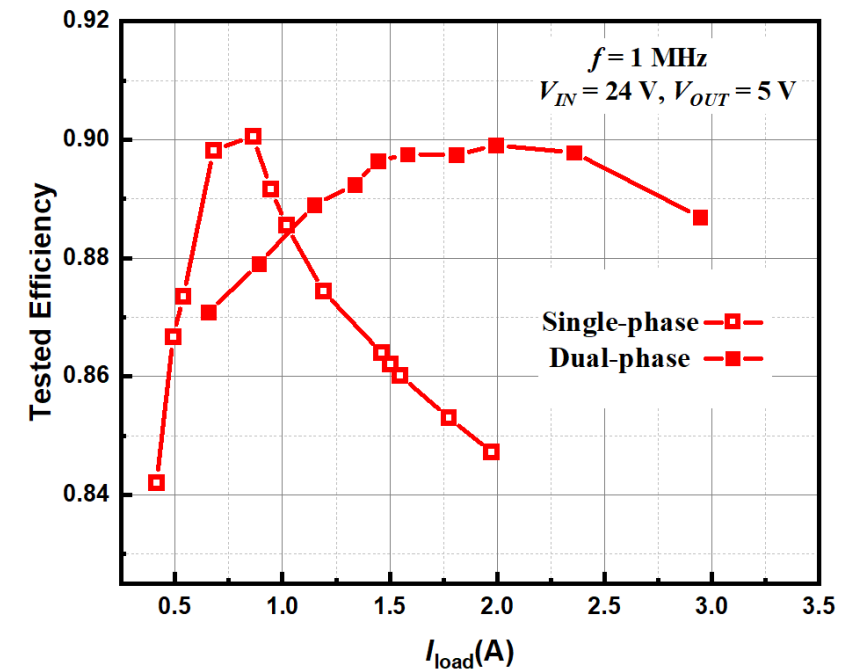
-- Higher efficiencies are realized over a wider load current range !



Dual phase buck converter output stage



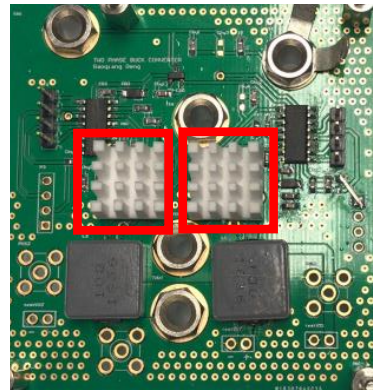
Test-bench using two modules



Efficiency plot



## Dual phase buck converter

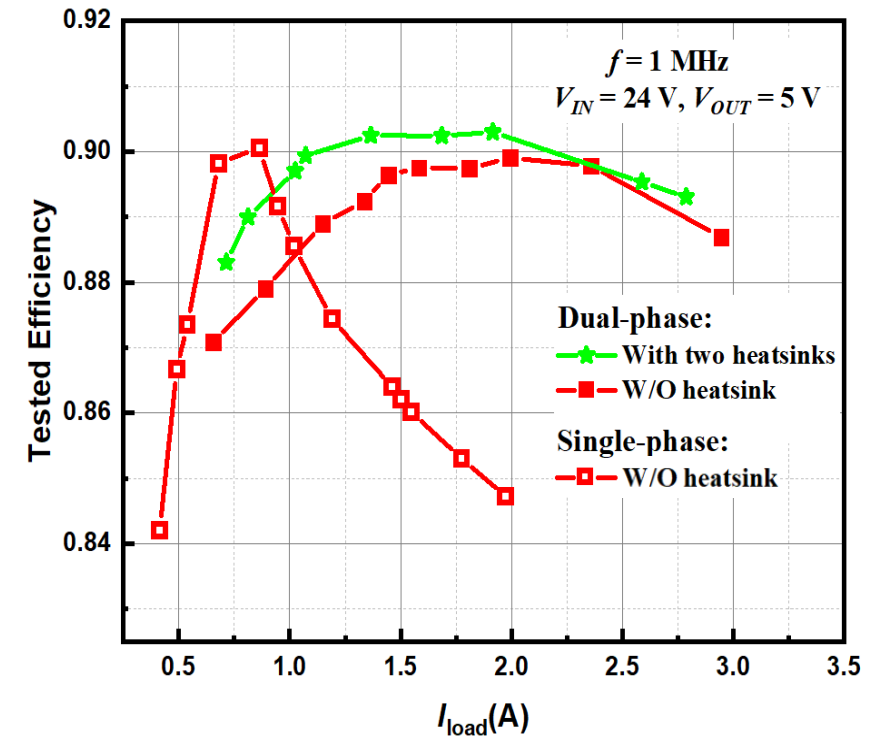


Without heatsinks



With two heatsinks

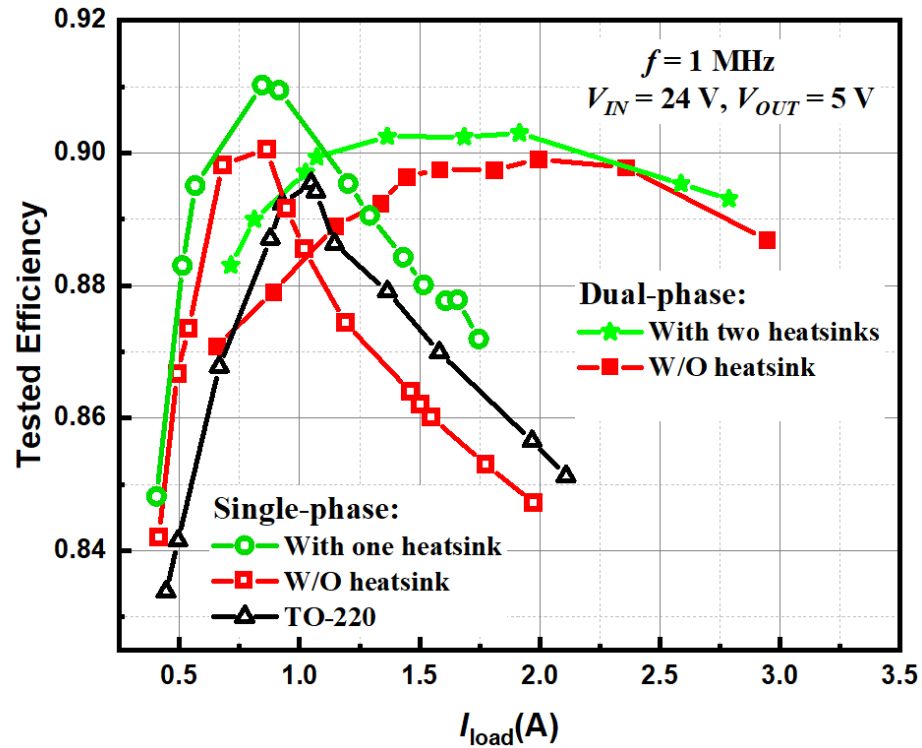
Convection cooling, Output power 9 W



Efficiencies are further increased by attaching heatsinks.



## Test-benches for all buck converters

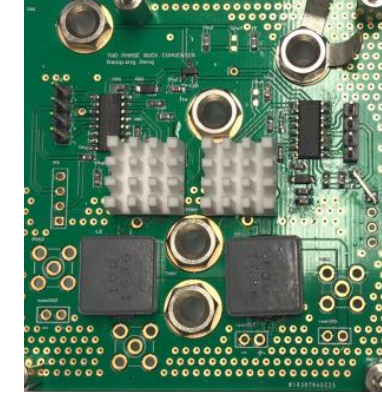


Convection cooling

### Dual phase

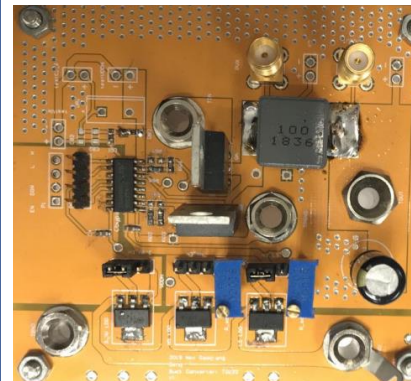


W/O heatsinks

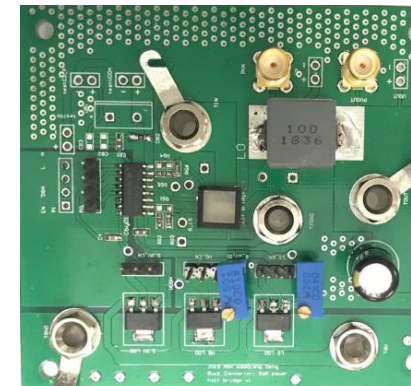


With heatsinks

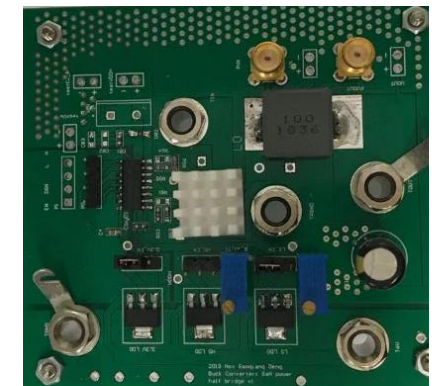
### Single phase



TO-220

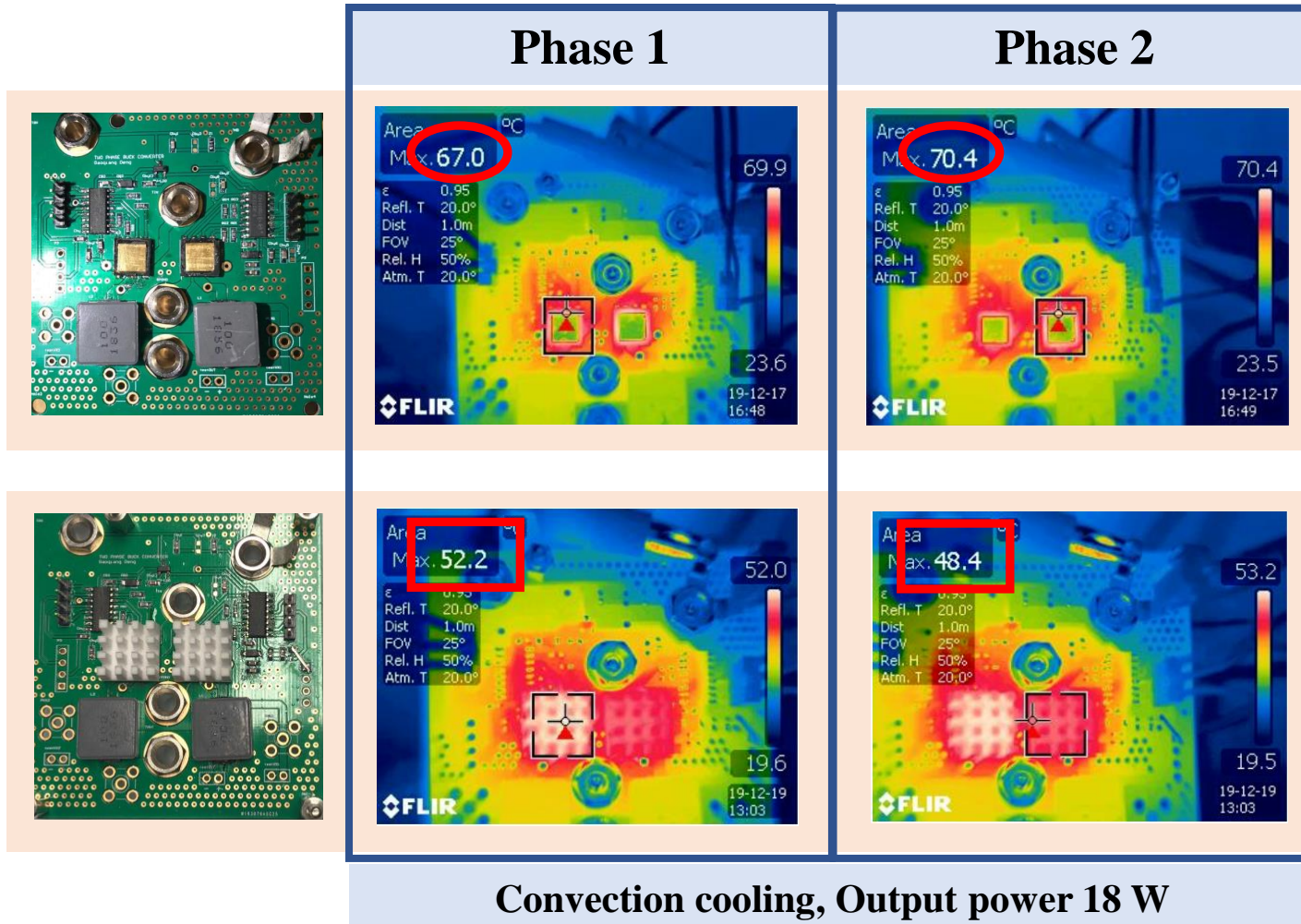


Module



Module with one heatsink

## Temperature differences between phases



Uneven convection airflow & current sharing



Increased peak temperature of PCB

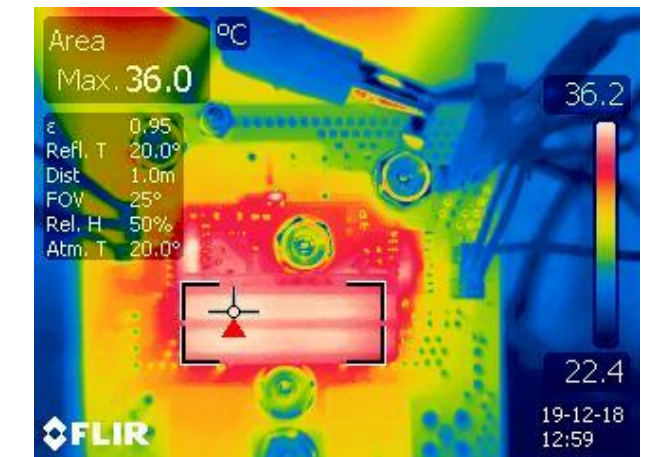
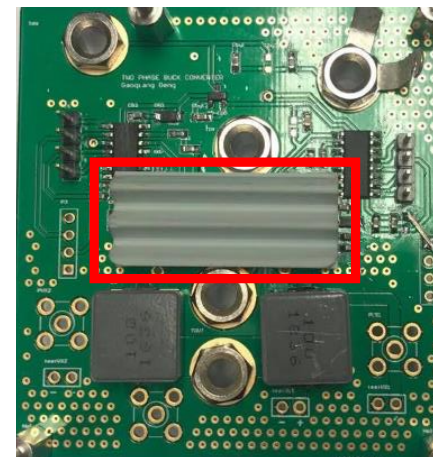
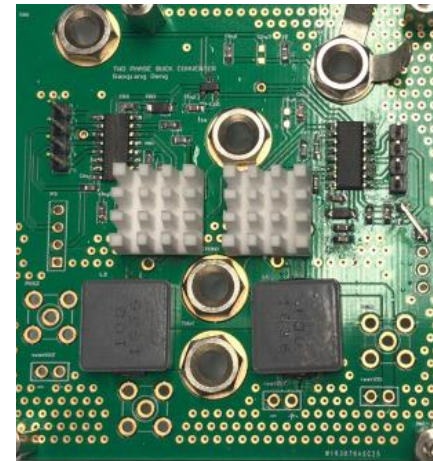
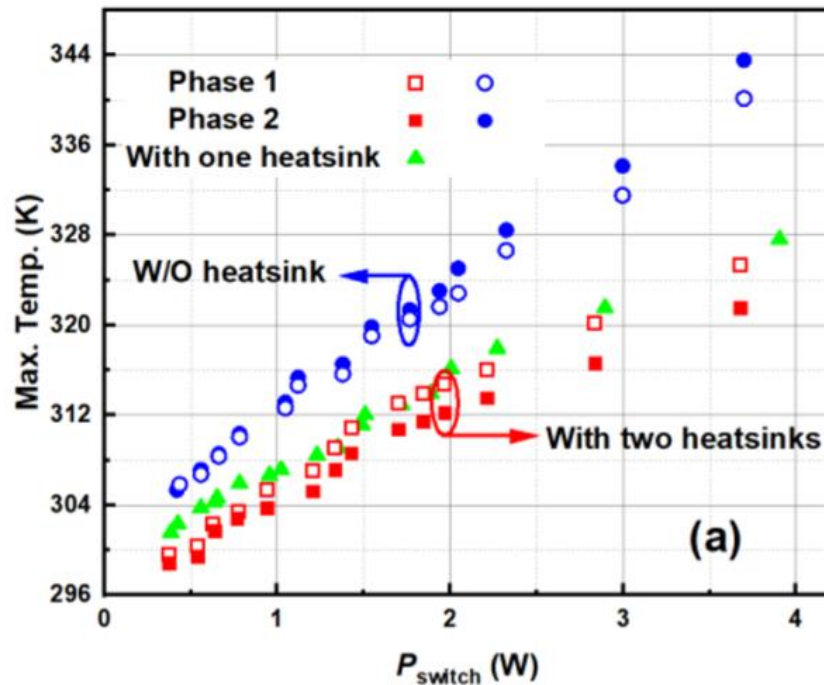


Reduced mean-time-before-failure & Reliability issues



## How to eliminate temperature variations

- Attach one heatsink on both modules
- Detect each phase's temperature and build a thermal management circuit



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## □ The proposed GaN power module

- Increased the power conversion efficiency under light loads
- Suppressed the ringing oscillation during high-frequency operation by minimizing the parasitics
- Conduction losses in the module are very sensitive to temperature

## □ Future work includes

- Optimizing the module package for better heat dissipation
- Building a thermal management circuit for multi-phase buck converters